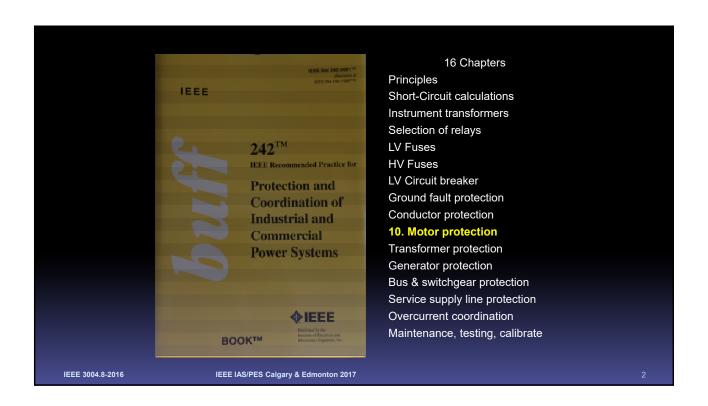
IEEE STD. 3004.8-2016 IEEE RP FOR MOTOR PROTECTION IN INDUSTRIAL & COMMERCIAL **POWER SYSTEMS OVERVIEW & WHAT'S NEW!**

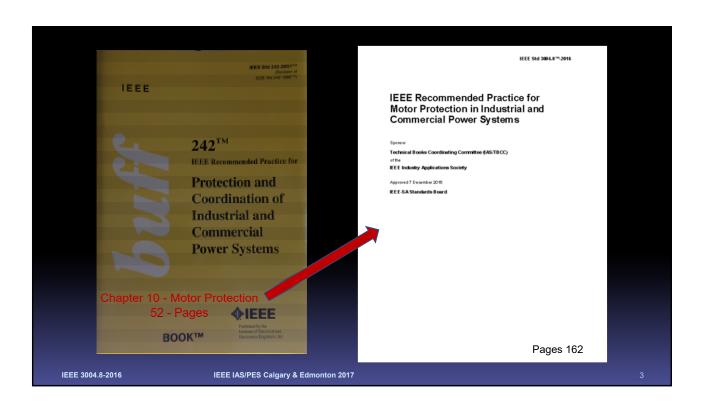
Lorraine K. Padden Senior Member, IEEE Padden Engineering, LLC paddeneng@aol.com

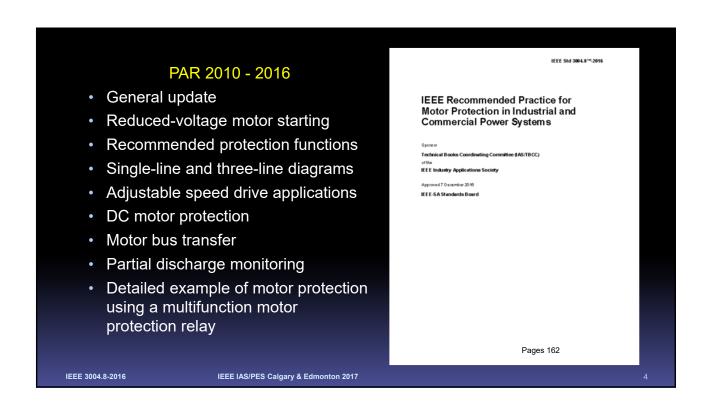
John A. Kay Fellow, IEEE **Rockwell Automation** jakay@ra.rockwell.com

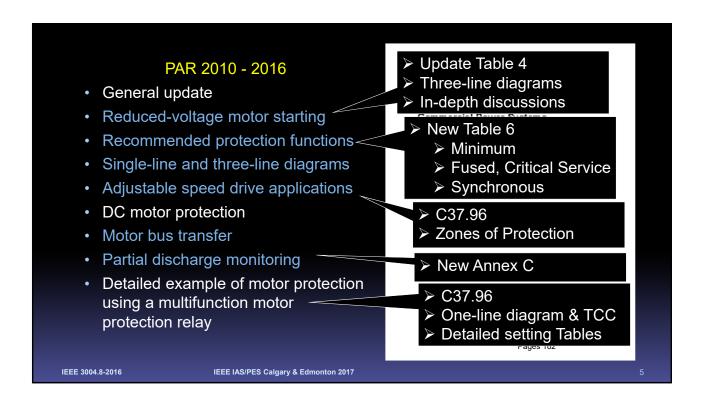


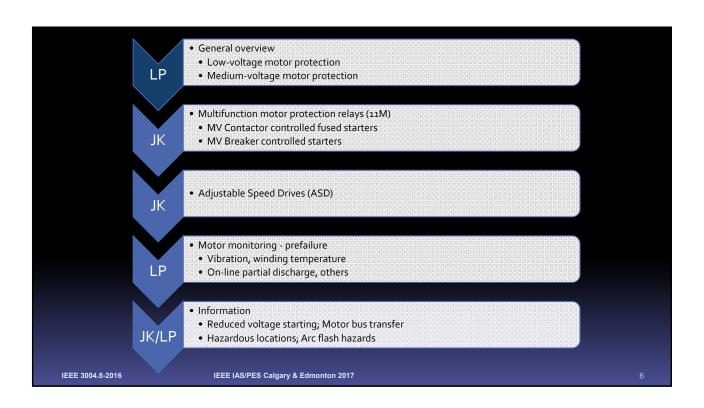
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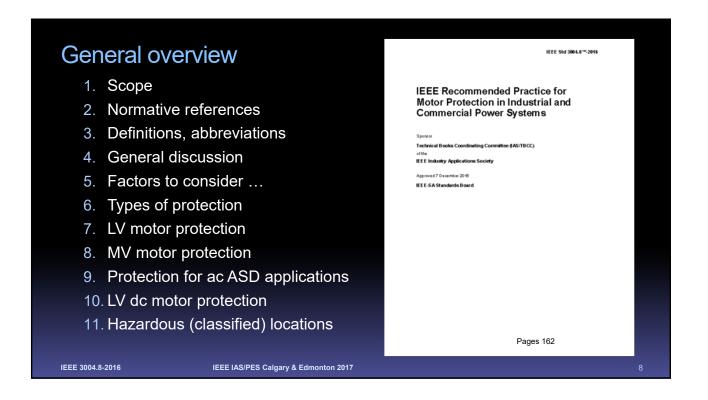




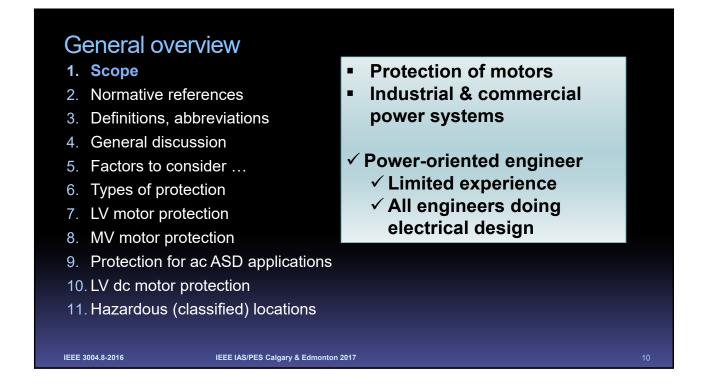








General overview IEEE Std 3004,8**-2016 > Annex A - Bibliography **IEEE Recommended Practice for** Motor Protection in Industrial and ➤ Annex B – IEEE device Commercial Power Systems designations Technical Books Coordinating Committee (IAS/TBCC) ➤ Annex C – Motor condition IEEE Industry Applications Society monitoring, on-line IEEE-S A Standards Board Annex D – Motor protection example ➤ Annex E – Motor open circuit time constant Pages 162 IEEE 3004.8-2016 IEEE IAS/PES Calgary & Edmonton 2017



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- Motor standards
 - ✓ IEEE Std. 841, TEFC
 - ✓ API 541, 546, 547
 - ✓ NEMA MG 1-2011
- Testing standards, IEEE
 - √ 112, Induction
 - √ 115, Synchronous
 - √ 43, Insulation resistance
 - √ 620, Thermal limit curves
 - √ 1349, Rotor temperature

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- Protection standards, IEEE
 - √ C37.2, Device functions
 - ✓ C37.96, Motor protection
 - √ C37.110, CTs for relaying
 - √ C62.21, Surge protection motors, 1000 V & greater
 - ✓ 3004.1, Instrument transformers
 - ✓ 3004.5, LV Circuit breakers

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- Equipment standards, IEEE
 - √ C37.06, Breaker >1000 V
 - ✓ C37.13, LVPCB
 - ✓ C37.14, DC power CB
 - ✓ C37.17, Trip systems
 - √ C37.46, HV Fuses
 - √ 1015, Blue Book, LVCB
 - √ 1683, MCCs, Electric hazard reducing

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- Equipment standards, NEMA
 - ✓ ICS 2, Contactors, controllers, overload relays; 600 V
- Equipment standards, UL
 - √ 347, MV AC contactors, controllers, and control centers
 - √ 845, MCCs

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Almost 60 definitions

√ normal operating condition:

As applied to motors, a normal operating condition is operating at rated full-load steady state conditions.

(See NFPA 70, National Electrical Code, Section 500.8(B)(5)) Locked-rotor, starting, single-phasing, and operating above base nameplate kilowatt or horsepower are not normal operating conditions

√ abnormal operating condition:

As applied to motors, including, but not limited to, starting, locked rotor, voltage unbalance, overload, and short-circuit. As applied to equipment in classified locations, equipment failure is considered to be an abnormal operating condition.

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Over 75 abbreviations

LV Low-voltage
MV Medium-voltage
FLC full-load current
LRC locked rotor current
FLT full load torque
CT Current Transformer
VT Voltage Transformer

SF service factor
TEFC totally enclosed fan-cooled

IOC instantaneous overcurrent
TOC time overcurrent

HRG High Resistance Ground
NEC® National Electrical Code

ASD adjustable speed drive

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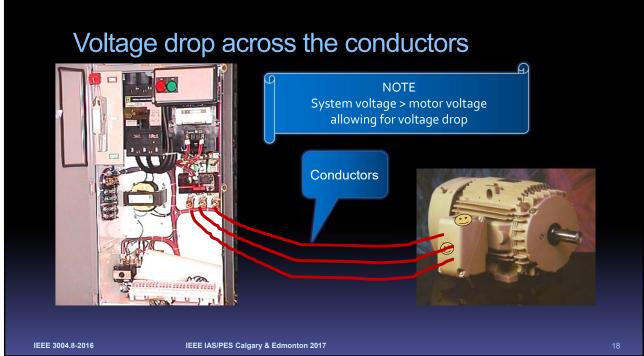


	Table 4 Namenlete :	reltante of LV materia	
	Table 1 Nameplate v		
	Nominal System Voltage	Typical Motor Nameplate Voltage	
	Single-phase System	Single-phase Motor	
	120 V	115 V	
	240 V	230 V	
	Three-phase System	Three-phase Motor	
	208 V	200 V	
	240 V	230 V	
	480 V	460 V	
	600 V	575 V	
_	Table 2 Nameplate v	oltage of MV motors	
	Nominal System Voltage	Typical Motor Nameplate Voltage	
	Three-phase System	Three-phase Motor	
	2400 V	2300 V	
	4160 V	4000 V	
	6900 V	6600 V	
	13.8 kV	13.2 kV	
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Table 3 Typical characteristics and applications of fixed frequency medium ac squirrel-cage induction motors (NEMA MG 10-2013)

Polyphase characteristics	Locked- rotor torque (percent rated load torque)	Pull-up torque (percent rated load torque)	Breakdown torque (percent rated load torque)	Locked- rotor current (percent rated load current)	Slip	Typical applications	Relative efficiency
Design A Normal locked rotor torque and high locked rotor current	70–275 ^a	65–190ª	175–300	Not defined	0.5–5%	Fans, blowers, centrifugal pumps and compressors, motor-generator sets, etc., where starting torque requirements are relatively low	Medium or high
Design B Normal locked- rotor torque and normal locked-rotor current	70-275ª	65–190ª	175–300ª	600–800	0.5–5%	Fans, blowers, centrifugal pumps and compressors, motor-generator sets, etc., where starting torque requirements are relatively low	Medium or high
Design C High locked- rotor torque and normal locked-rotor current	200–285ª	140–195ª	190–225ª	600–800	1–5%	Conveyors, crushers, stirring machines, agitators, reciprocating pumps and compressors, etc., where starting under load is required	Medium
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Design D High locked- rotor torque and high slip IEC Design H High locked rotor torque and high locked	Not defined	275	600–800	≥5%	High peak loads with or without flywheels such as punch presses, shears, elevators, extractors, winches, hoists, oil-well pumping and wire- drawing machines Conveyors, crushers,	Medium
High locked rotor torque and 200—289					Conveyors, crushers.	
rotor current	5ª 140–195ª	190–225ª	800–1000	1–5%	stirring machines, agitators, reciprocating pumps and compressors, etc., where starting under load is required	Medium
IEC Design N Normal locked- rotor torque and high locked rotor current	a 60–140 ^a	160–200³	800–1000	0.5–3%	Fans, blowers, centrifugal pumps and compressors, motor- generator sets, etc., where starting torque requirements are relatively low	Medium or high

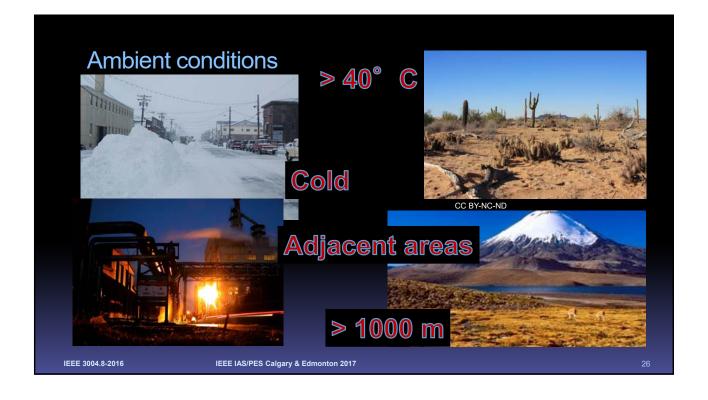
General overview 1. Scope 5.1 Motor characteristics 5.2 Motor starting conditions 2. Normative references 5.3 Ambient conditions 3. Definitions, abbreviations 5.4 Driven equipment 4. General discussion 5.5 Power system quality 5. Factors to consider ... 5.6 Motor importance 5.7 Load side faults for motor controllers 6. Types of protection 5.8 Ground faults 7. LV motor protection 5.9 Maintenance capability & schedule 8. MV motor protection 5.10 Service factor 9. Protection for ac ASD applications 5.11 Application considerations 5.12 Motor & conductor protection 10. LV dc motor protection 5.13 Fixed capacitor applications 11. Hazardous (classified) locations IEEE 3004.8-2016 IEEE IAS/PES Calgary & Edmonton 2017

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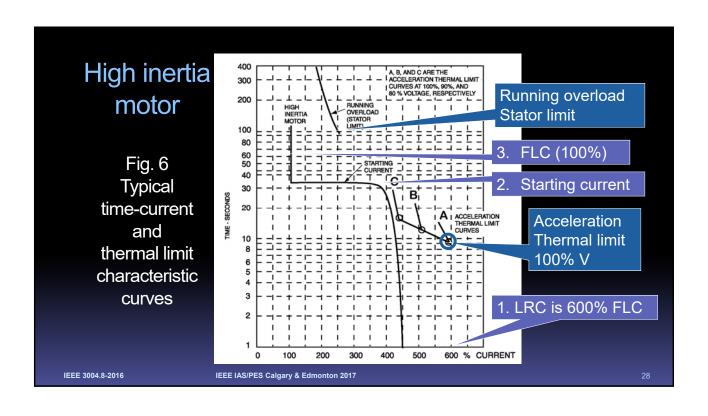
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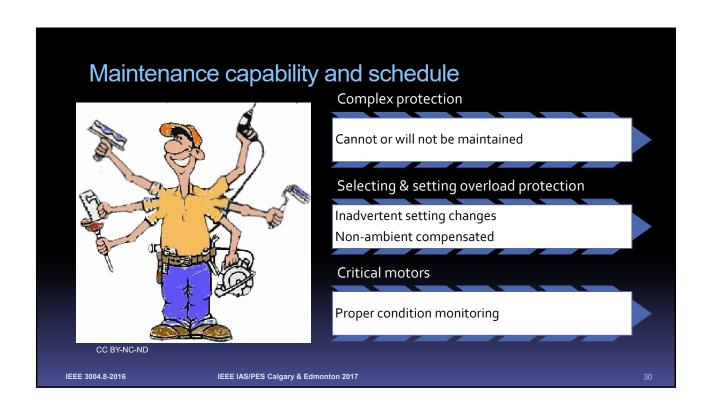
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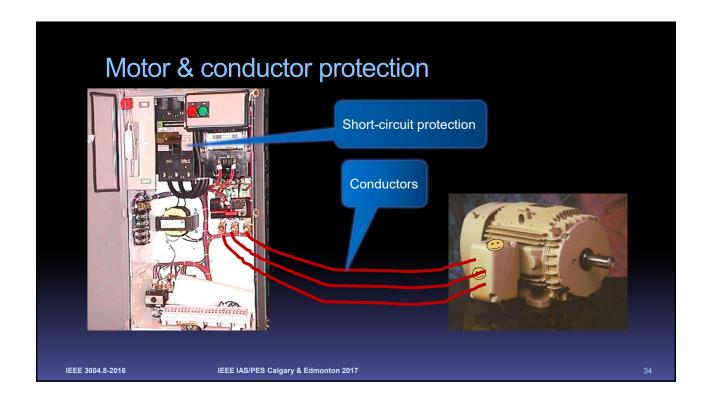
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Fixed capacitor applications

- Modify overload setting if on the load side
- Extend the motor open circuit time constant
- Motor capacitor application may not be recommended for reacceleration motors



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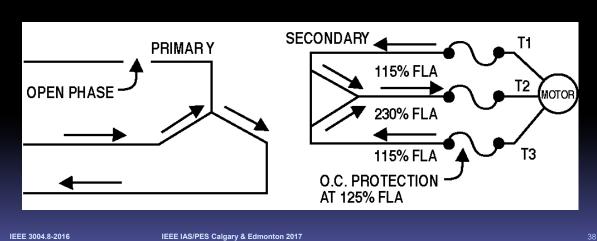
- Recommended protection functions
 - √ New Table 6
 - ✓ Minimum
 - √ Fused, Critical Service
 - √ Synchronous
- Single-line and three-line diagrams

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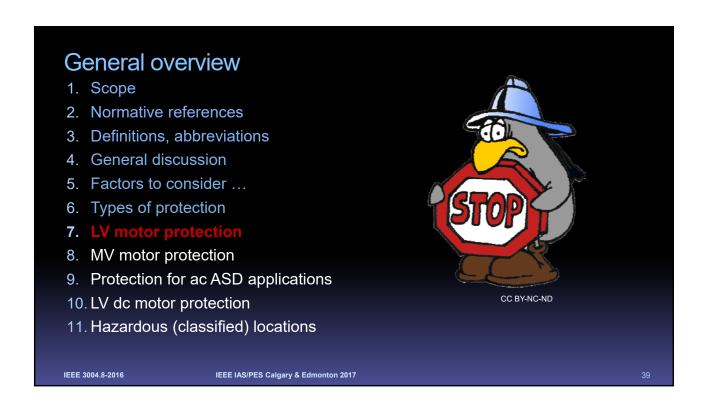
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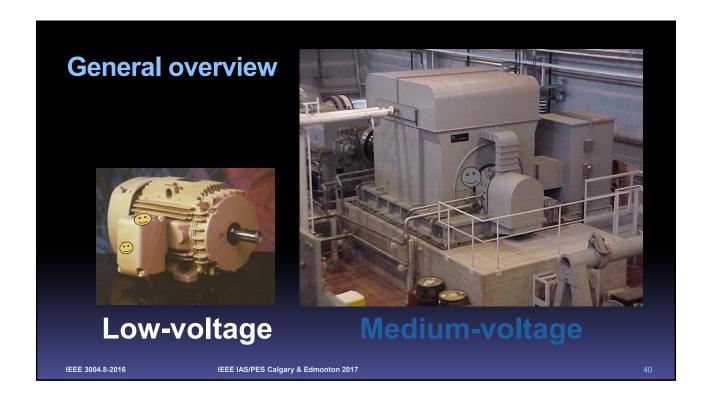
Fig. 10 Loss-of-phase current

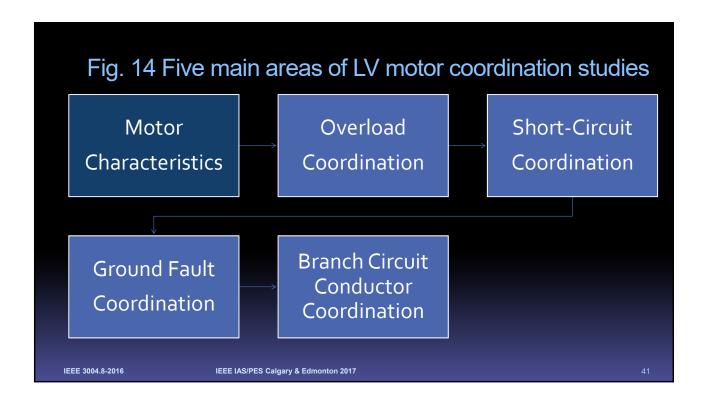
b) wye-delta connected transformer with wye or delta connected motor

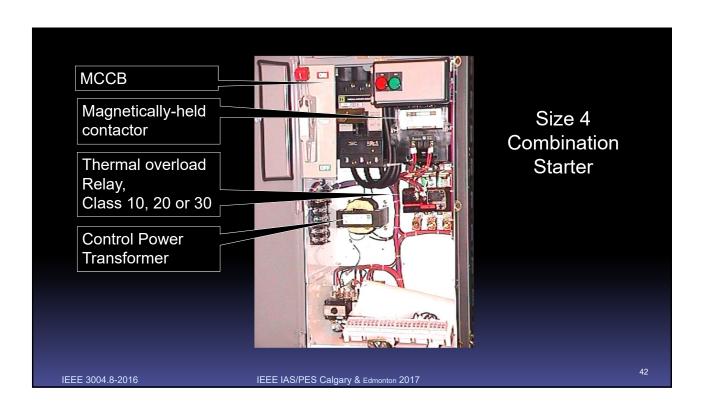


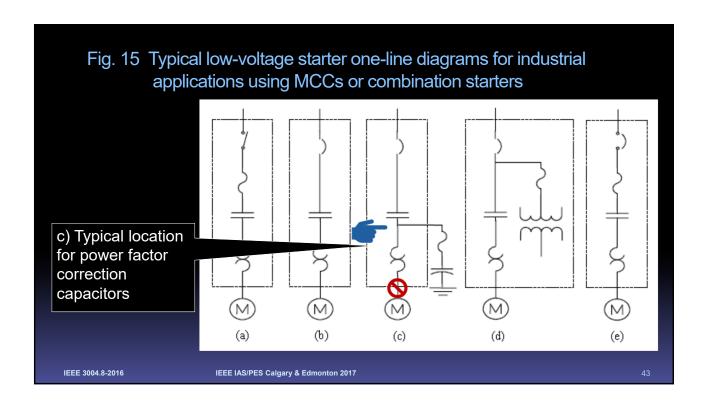
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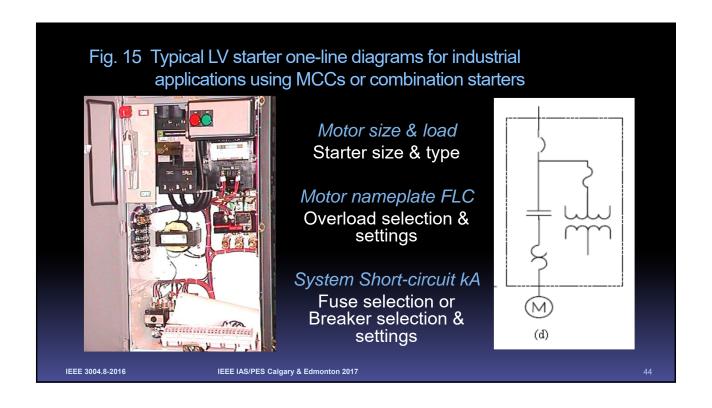




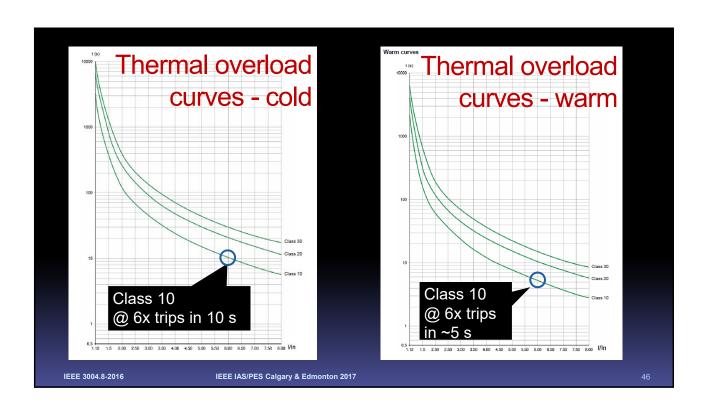


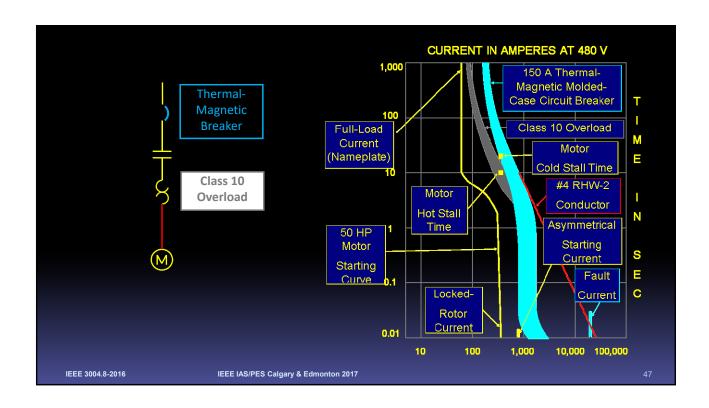


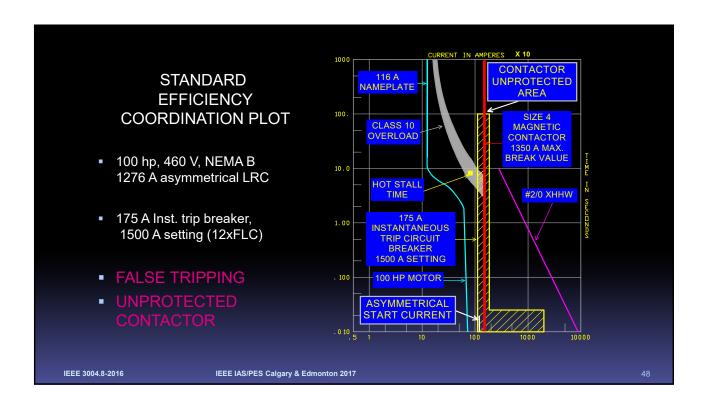










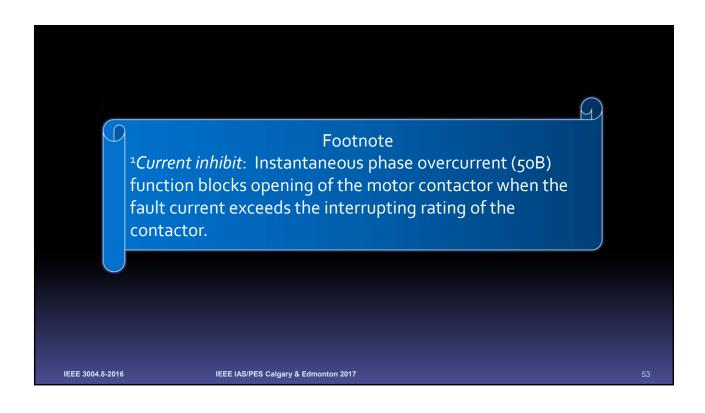


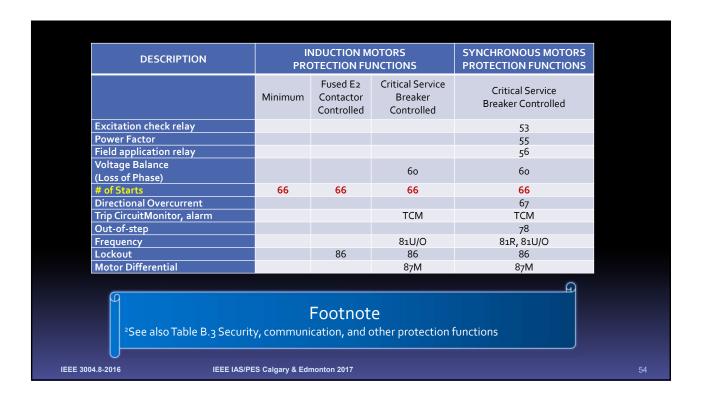


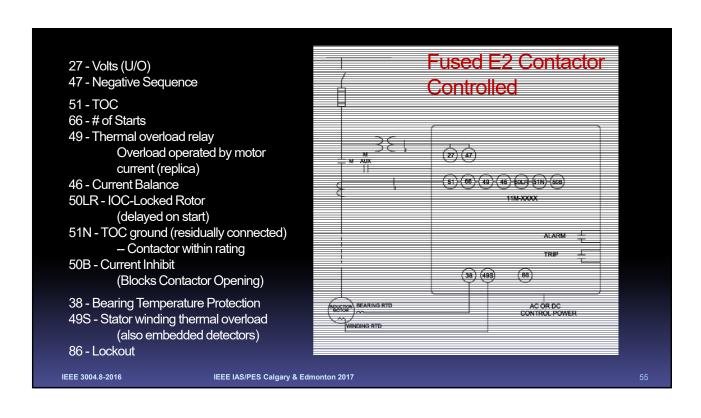


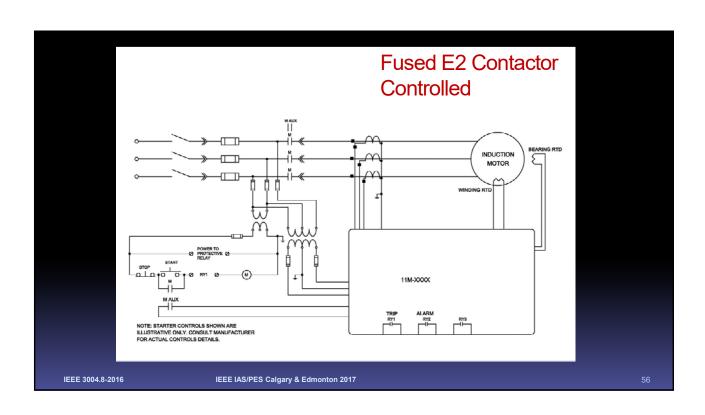
DESCRIPTION	INDUCTION MOTORS PROTECTION FUNCTIONS			SYNCHRONOUS MOTORS PROTECTION FUNCTIONS	
	Minimum	Fused E2 Contactor Controlled	Critical Service Breaker Controlled	Critical Service Breaker Controlled	
Distance Relay				21 (or 51V)	
Volts (U/O)	27	27	27/59	27/59	
Directional Power				32	
Undercurrent			37	37	
Bearing Temperature Protection		38	38	38	
Vibration Protection			39	39	
Loss of Field				40	
Current Balance		46	46	46	
Negative Sequence		47	47	47	
Incomplete Sequence				48	
Thermal overload relay Overload operated by motor current (replica),	49	49	49	49	
Stator winding thermal overload (also embedded detectors)	49S	49S	49S	49S	

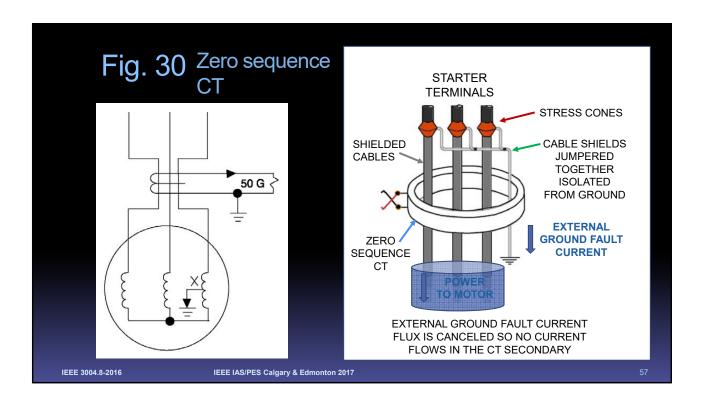
DESCRIPTION		NDUCTION M DTECTION FU	SYNCHRONOUS MOTORS PROTECTION FUNCTIONS	
	Minimum	Fused E2 Contactor Controlled	Critical Service Breaker Controlled	Critical Service Breaker Controlled
Breaker Failure (breaker only)			50BF	50BF
IOC ground (zero sequence CT) (delayed on start) - Breaker Trip or - Vacuum Contactor within rating	50 G	50 G	50 G	50 G
TOC ground (residually connected) - Breaker Trip or - Vacuum Contactor within rating	51N	51N	51N	51N
IOC-Locked Rotor (delayed on start)		50LR	50LR	
TOC (V-voltage restrained)	51		51	51V (or 21)
Short-circuit	Fuse or Breaker, 50	Fuse	50	50
Current Inhibit (Blocks Contactor Opening) ¹	50B	50B		

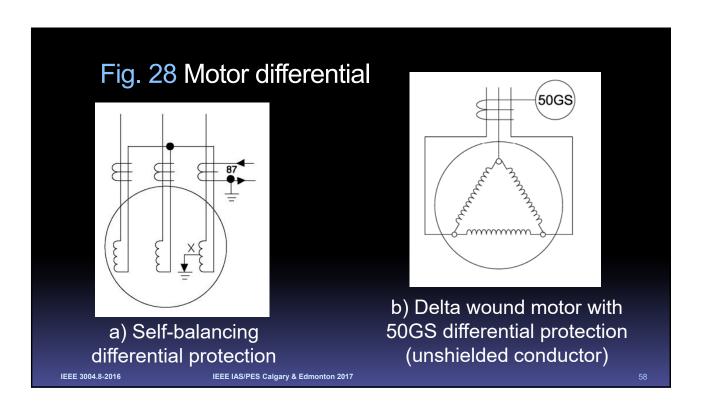


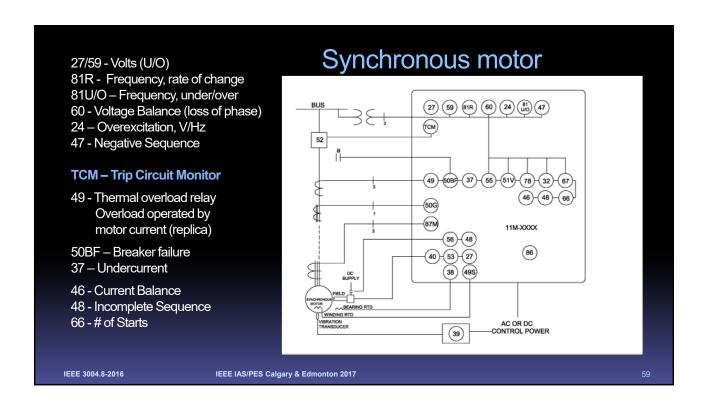


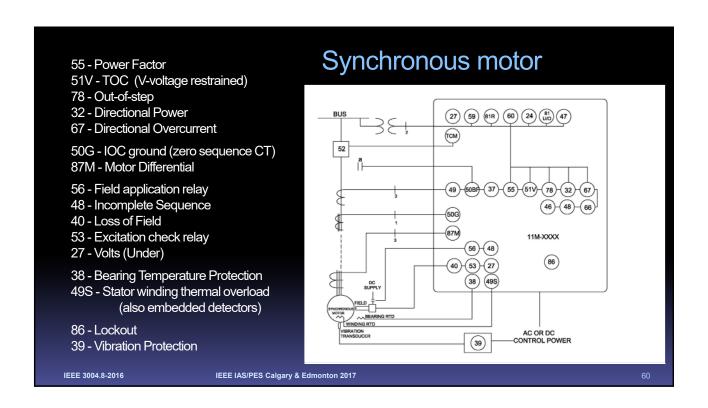


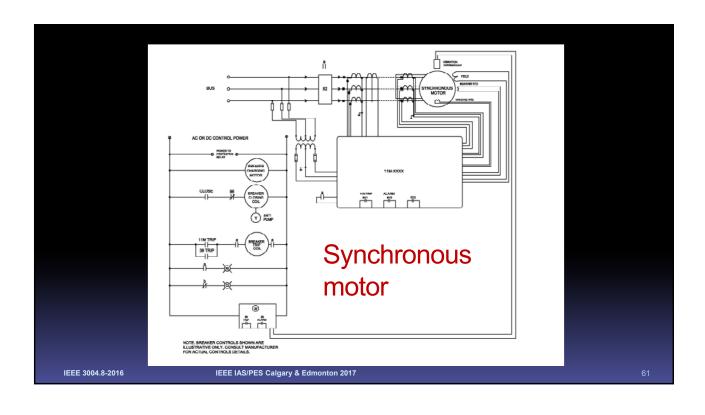




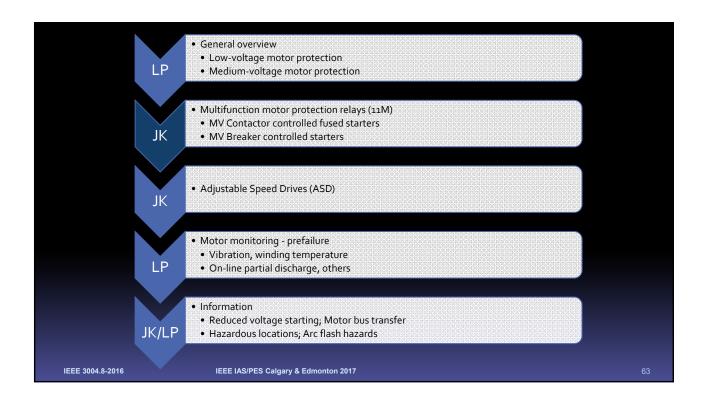


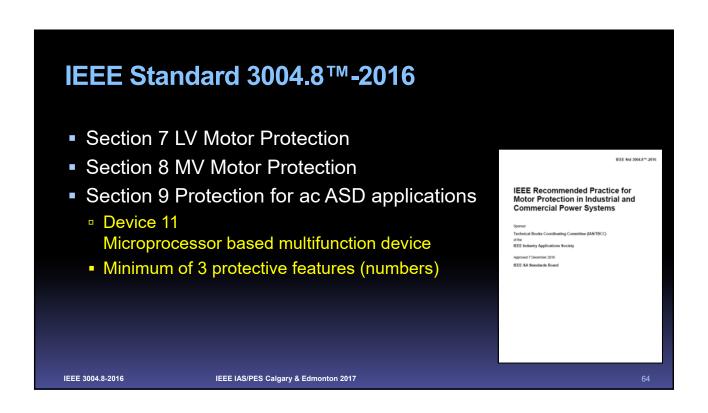












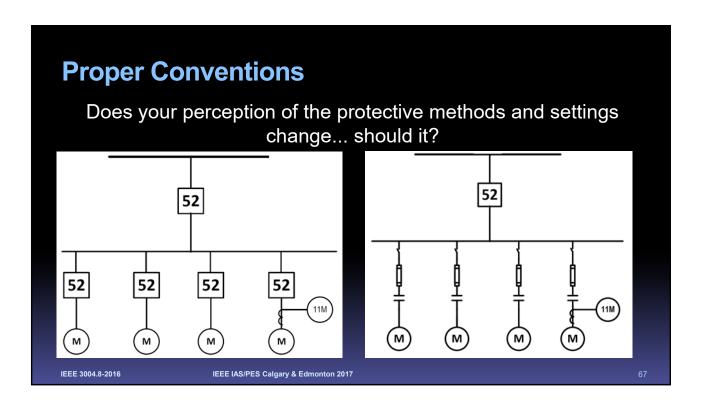


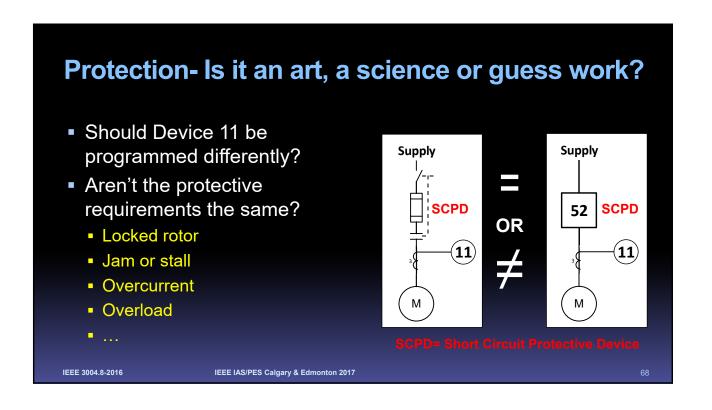
Protection- Is it an art, a science or guess work?

- Multifunction protection devices (MPR) are common place...
- Many vendors with many options... more everyday
- Most users only use between 20-30% of the these devices capabilities!
- Which protective elements are really important?
- Are there different protective setting based on switching devices?
- Are there setting differences based on control and application?

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Protection- Is it an art, a science or guess work?

- The SCPD and Device 11 must be coordinated so that each operates in its appropriate protection range
- Contactors are only rated for interrupting currents typically X10-15 their continuous rated current, e.g. 400A x 4000-6000A
- The SCPD must operate before the Device 11 opens the contactor
- The contactor will be damaged if it is forced to interrupt I > its interrupting rating

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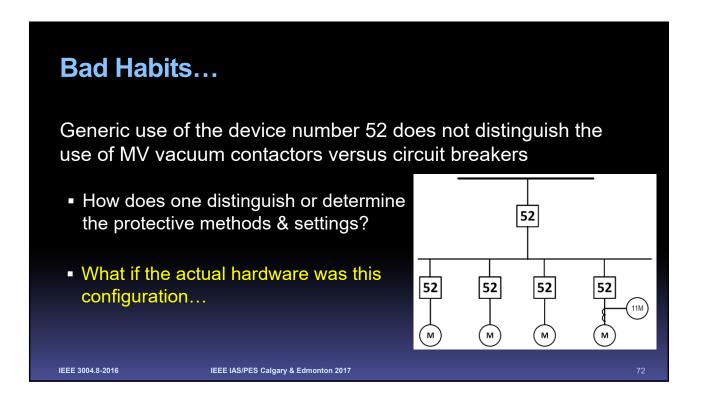
Contactors versus Breakers

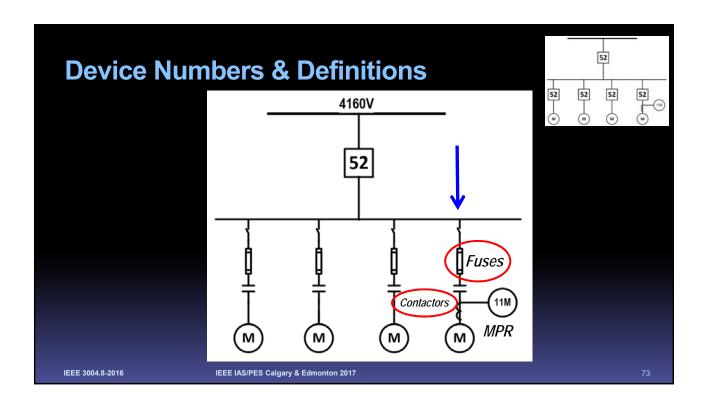
- No protection element should trigger opening the contactor unless the fault current is less than contactors interrupting capabilities
- Same applies to differential protection relays used with contactors
- Fused contactor arrangements must be coordinated to support this condition

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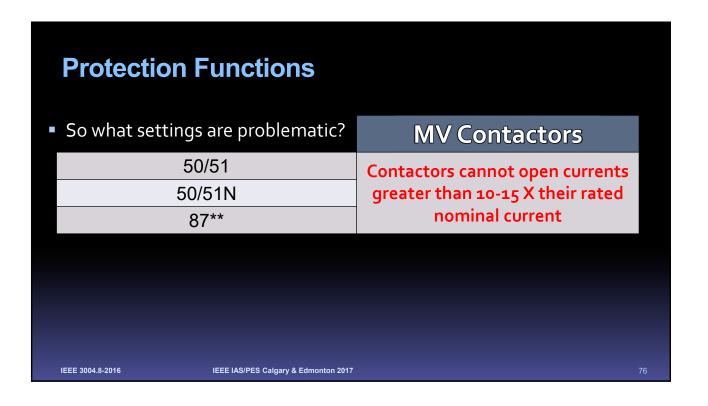
TYPICAL FAULT CLEARING TIME COMPARISON AT 20 X RATED CURRENT Vacuum Contactors (UL 347 Class E2 controller) Current-limiting fuses clearing time is < ½ cycle Vacuum Circuit Breakers 3 or 5 cycle interrupting time, plus_the relay trip latency



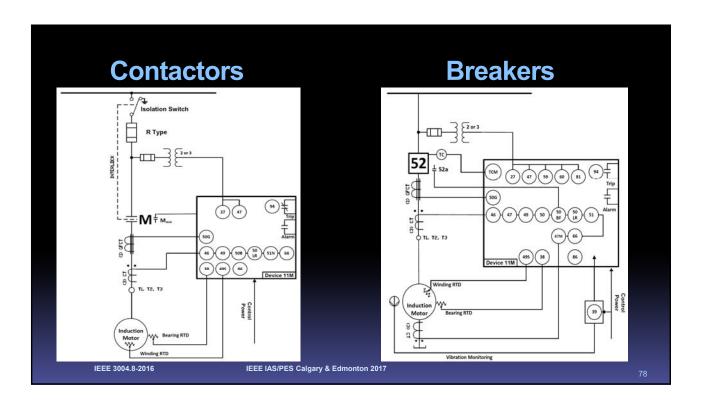


Applications Best Suited for Switching Device					
MV Circuit Breaker	MV Contactors				
Disconnecting means for power bus	Motor control <800A				
Substation switching	Controlling distribution transformers				
Main-Tie-Main bus configurations	High duty switching requirements				
Very large electric machines	Bypass for ASD or Soft Starters				
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Protection Functions		
So where are the issues?	MV Circuit Breakers	MV Contactors
Can handle system S.C. current	Yes	No
Can handle overload currents	Yes	Yes
Can switch and carry rated current	Yes	Yes
Permitted to open under emergency high current conditions	Yes	No
Requires a supplemental S.C. protective device	No	Yes
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Protection FunctionsSo what settings are problematic?	MV Contactors				
50/51 Contactors cannot open currents greater than 10-15 X their rated nominal current					
**Most manufacturers of MPRs, with Device 87 ca user guides related to the use of the 87 function Problem is - FEW USERS	on with fused contactors but ignore the 50/51				
e.g. "Care must be taken when enabling (contactor or circuit breaker) is not rated a should be disabled A low level different in an instant"	to break potential faults, the feature				
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Conclusions & Recommendations

- Know the type of switching device being applied
- Use the proper symbology on drawings
- Know the interrupting rating of the switching devices
- Select proper protective elements for the switching device
- Insure protection settings are within rating of the switching device ...

Assumptions in Protection Lead to Unsafe Conditions!

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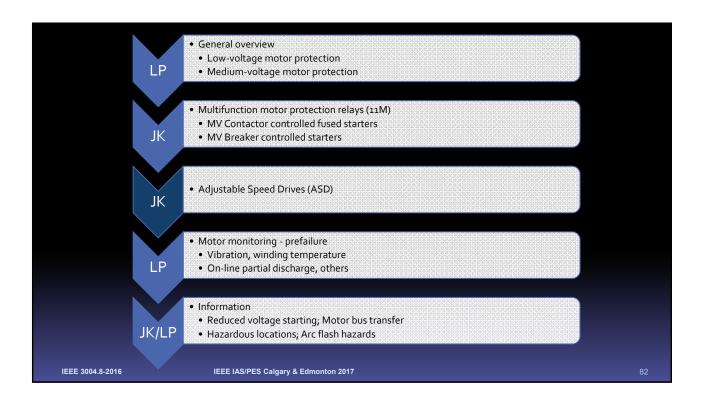
Conclusions & Recommendations

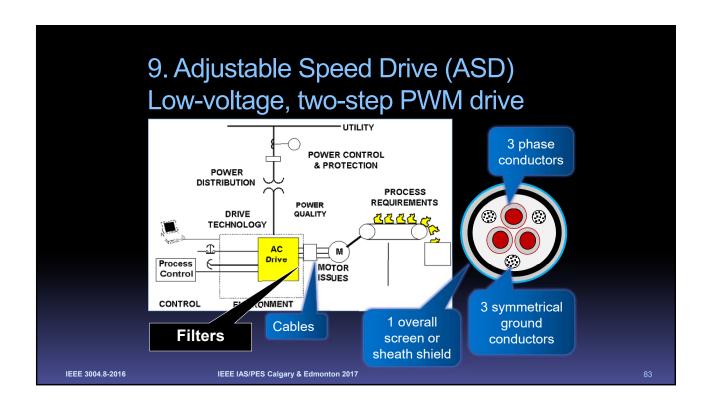
- One-line diagrams form the foundation for selecting the proper protective device settings
- One-line diagrams must clearly illustrate the difference between the two switching methods
- NEMA ICS 19-2002 uses "M" as the designation for the Main Contactor
- Do not use device 52 generically!

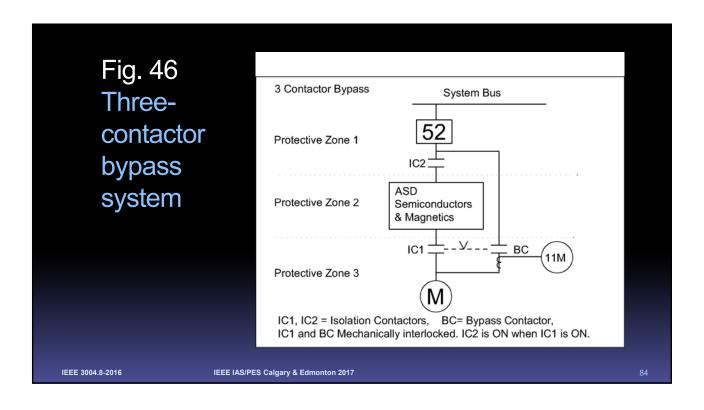
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- ASDs create additional challenges for external motor protection that are not present in direct, line connected, motors
- Some protection challenges are solved by "new" protection elements available in an electronic motor protection relay... but is it marketing hype?
- Fundamental frequency measurements are used in most protection elements in MPR
- ASD can rapidly change from the fundamental frequency

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The challenges of motor protection on ASD

- The synthesized sine waves produced by some ASD topologies and vendor products can contain significant harmonic content
- True RMS measurements can properly account for the motor heating caused by harmonic currents
- Not all protection relays use true RMS (fundamental plus some of the harmonics) for protection
 - Can the relay measure the THD?

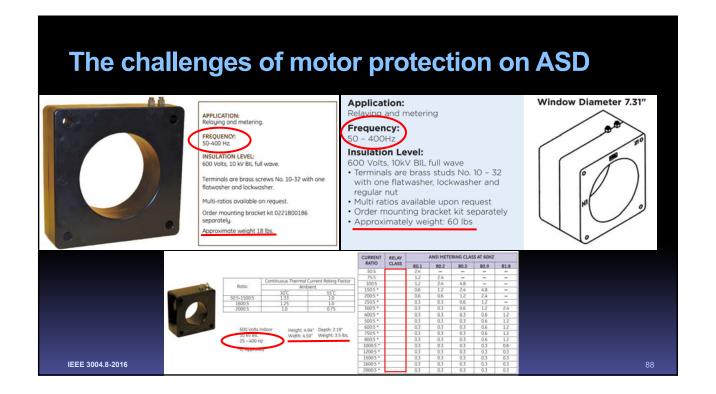
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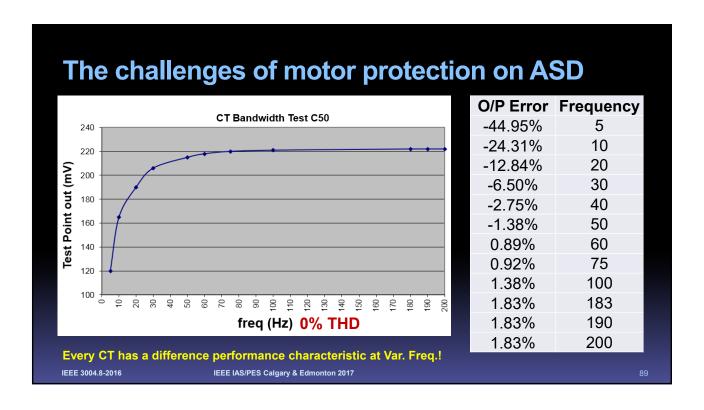
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- The bigger challenge is not the MPR performance but having the measuring devices on the output, i.e. CTs & VT/PTs
- Poor data quality = poor protection
- Magnetic core based measurement devices are generally optimized to work based on a specific fundamental frequency
- CT designs optimized for use at 40 (50) 400Hz
- PT/VT optimized for a specific fundamental frequency +/-%

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- Lots of variability between CT core designs and materials
- At prolonged low frequency the saturated core actual has a significant temperature rise
- Rise varies significantly between materials and construction of the core

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- Almost all motor protective algorithms in MPRs are based around a fixed frequency (non-VFD) protection
- Use positive and negative-sequence components as inputs to a first-order thermal model from which the rotor and stator heating are calculated
- ASD use hall effect style sensors which are accurate to very low frequency levels and high spec

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- Certain MPR protective features must be disabled or set differently to work with the ASD
- Redundancy between the protection provided by MPR and the ASD leads to unnecessary added troubleshooting
- Having more devices to troubleshoot and potentially adding false positive indication for MPR's that have not been properly set.

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Motor Differential Protection

- There is a limitation in the ability to detect differential currents at lower frequencies
- The inherent characteristic of current transformers prevent accuracy
- Some ASDs have flux and DC unbalance protection schemes which may be used either on their own or in conjunction with the core balance approach since the accuracy particularly at lower speeds is superior
- These protective functions are embedded in the ASD control, do not require CTs in the motor terminal box or the associated conduit and wiring runs between the drive and motor which is particularly significant when the motor is at a significant distance away from the controller.

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Load side protection on ASD using MPR

- Leads to many complications beyond those typically addressed for across-the-line applications
- Each protective function has to be evaluated independently
- Most standard MPRs are not equipped with the capability to analyze a power signal with these varying conditions
- The protective functions within the drives themselves eliminate complexity and avoid nuisance trip conditions
- If the functions are not available in the drive apply external protective relaying capable of analyzing the variable conditions present downstream of the drive, e.g.RTD

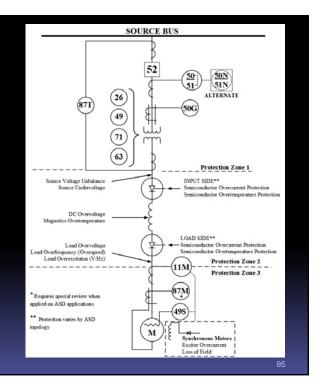
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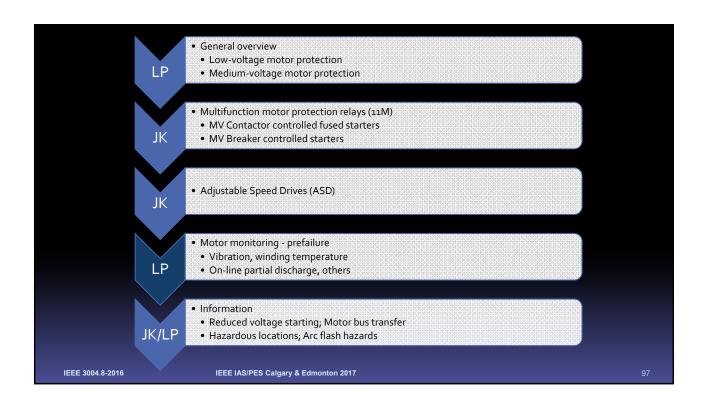
Recommendations

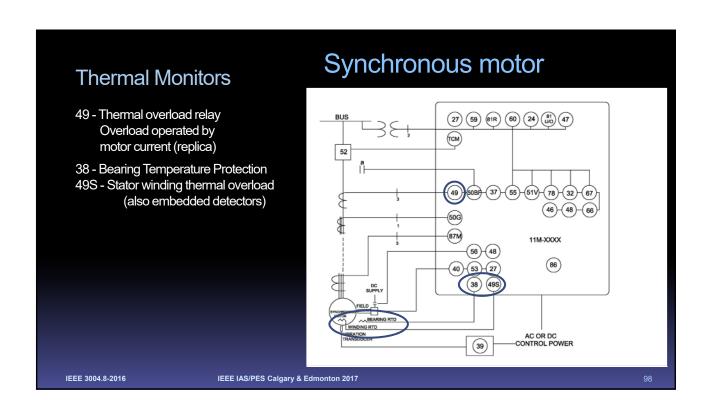
- Best motor protection provided by the drive's control!!!
- CT performance concerns at low frequency/high harmonic content
- Self-balancing differential protection (Device 87M) best but limitation on detecting at lower frequencies due to the inherent characteristics of current transformers

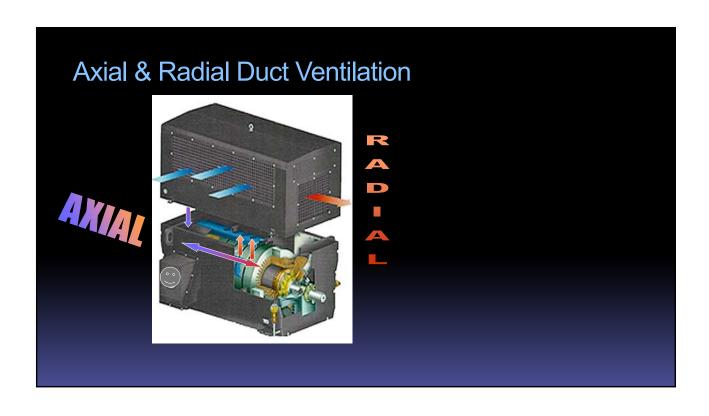
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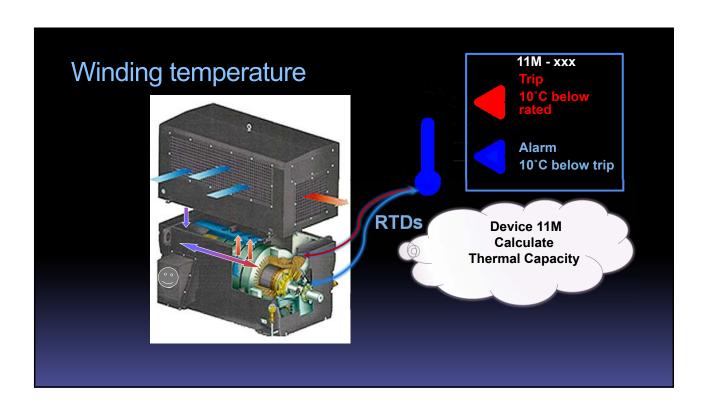


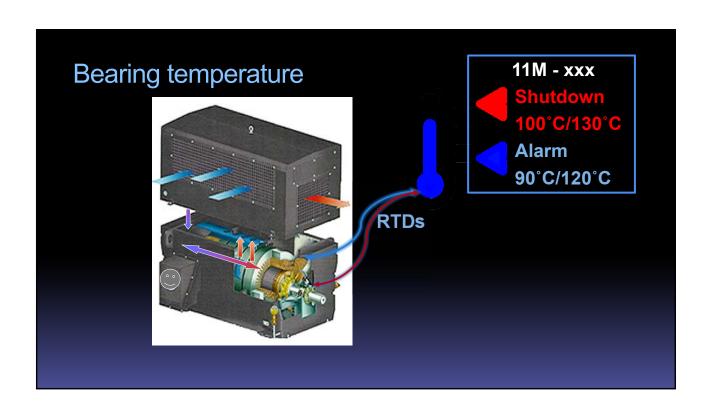


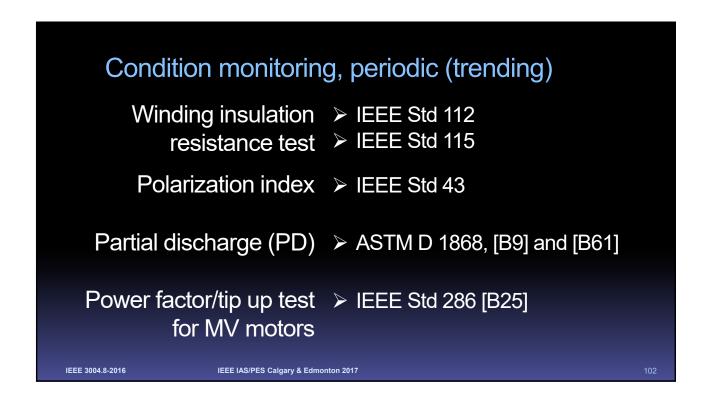












Condition monitoring, on-line (trending)

- √Vibration analysis (8.5.5)
- ✓On-line partial discharge (OLPD) (8.5.4.6 and C.1) [8 bibliography references]
- ✓ Monitoring motor insulation on-line (C.2)

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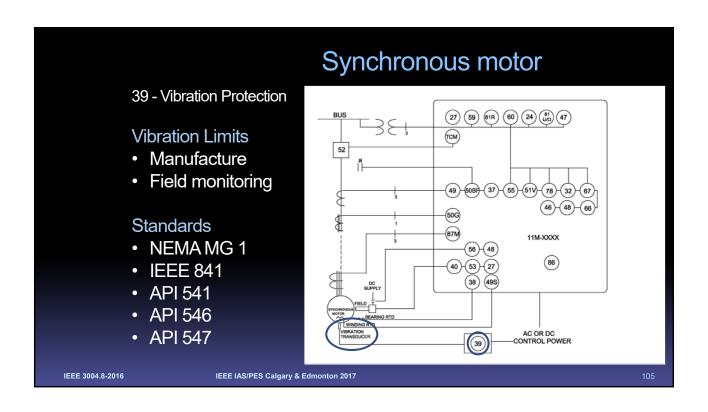
8.5.5 Vibration

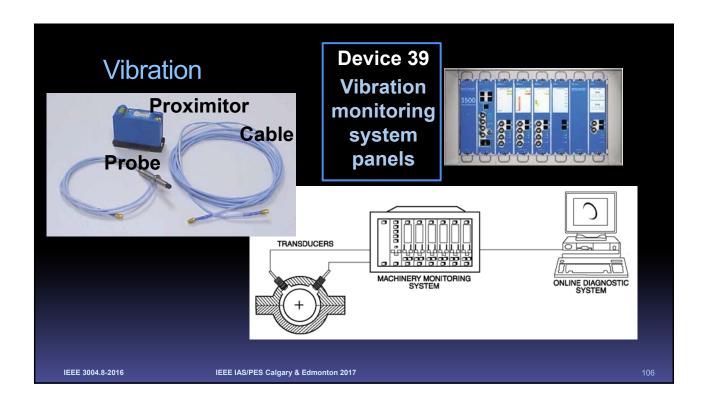
Bearing fail

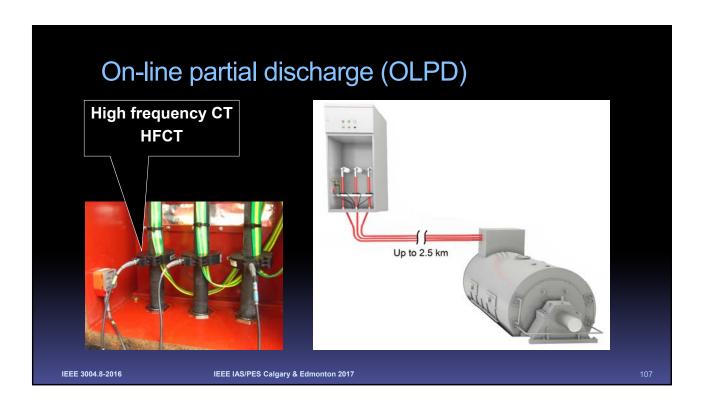
Shaft break

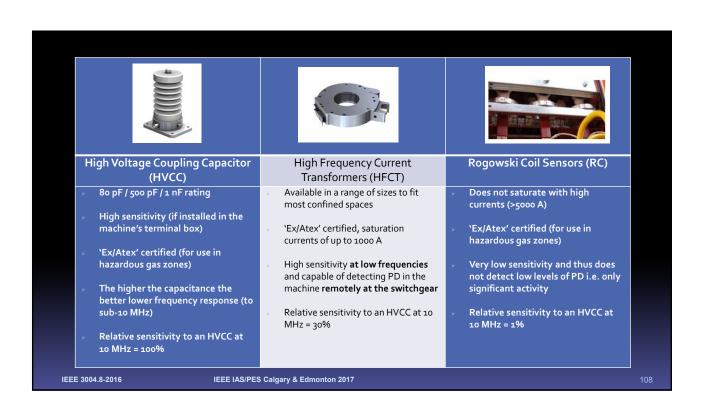
Staff break

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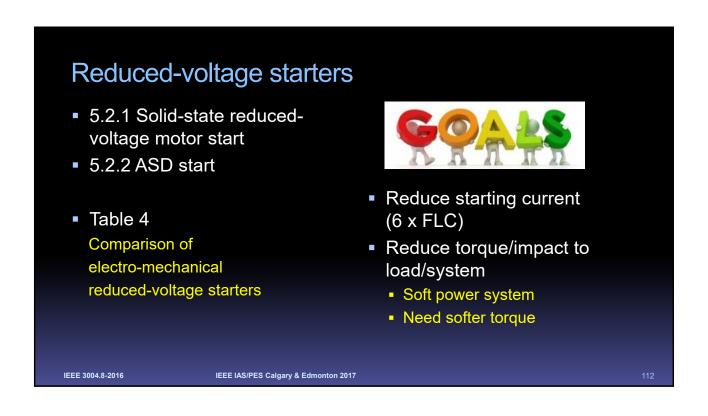




Condition AssessmentPeak PD Level (nC)OLPD Activity (nC/cycle)Excellent< 2< 50Good2-450-99Average4-10100-249Still Acceptable10-15250-499Inspection Recommended15-25500-999	ole C.1 OLPD guideline levels for MV motors in the 10 kV to 15 kV c					
Good 2-4 50-99 Average 4-10 100-249 Still Acceptable 10-15 250-499 Inspection Recommended 15-25 500-999			· · · · · · · · · · · · · · · · · · ·			
Average 4-10 100-249 Still Acceptable 10-15 250-499 Inspection Recommended 15-25 500-999	Excellent	< 2	< 50			
Still Acceptable 10 – 15 250 – 499 Inspection Recommended 15 – 25 500 – 999	Good	2 – 4	50 – 99			
Inspection Recommended 15 – 25 500 – 999	Average	4-10	100 – 249			
	Still Acceptable	10 – 15	250 – 499			
Uproliable	Inspection Recommended	15 – 25	500 – 999			
> 25 > 1000	Unreliable	> 25	> 1000			







28% 25%	45% 42%	67% 64%	65% Tap 65% 42%	80% Tap 80% 64%	2-step 60%‡ 50%	Wye start- delta run 33 ¹ / ₃ %
	.5	ŕ	J			
25%	42%	64%	42%	64%	50%	33 ¹ / ₃ %
Increases slightly with speed		Increases greatly with speed				
Second in order of smoothness		Smoothest of reduced-voltage types in Table 4. As motor gains speed, current decreases. Voltage drop across resistor decreases and motor terminal voltage increases		Fourth in order of smoothness	Third in order of smoothness	
,	Adjustable within limits of various taps		Adjustable within limits of various taps			Fixed
		Adjustable withi various ta	Adjustable within limits of various taps	in Table 4. As me current decrease across resistor determinal volt Adjustable within limits of various taps in Table 4. As me current decrease across resistor determinal volt Adjustable within limits of various taps	in Table 4. As motor gains speed, current decreases. Voltage drop across resistor decreases and motor terminal voltage increases Adjustable within limits of	in Table 4. As motor gains speed, current decreases. Voltage drop across resistor decreases and motor terminal voltage increases Adjustable within limits of various taps Adjustable within limits of various taps

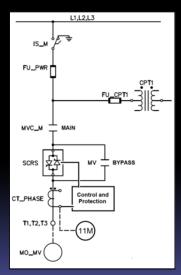
Solid-State Reduced-Voltage Starting

- ASD are the premium solution for reduced voltage starting
 - Very large
 - Very costly
 - Generally way more machine than is needed
- Internal ASD protection elements adequate for motor protection except usually additional 49S/38/39 protection required

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Solid-State Reduced-Voltage Starting

- Fundamental motor protection elements on board in control and protection modules
- A device 11 (or others) may provide additional protection such additional stator, bearing or vibration protection
- Use caution when there are duplicate protection elements between the multiple protection devices...



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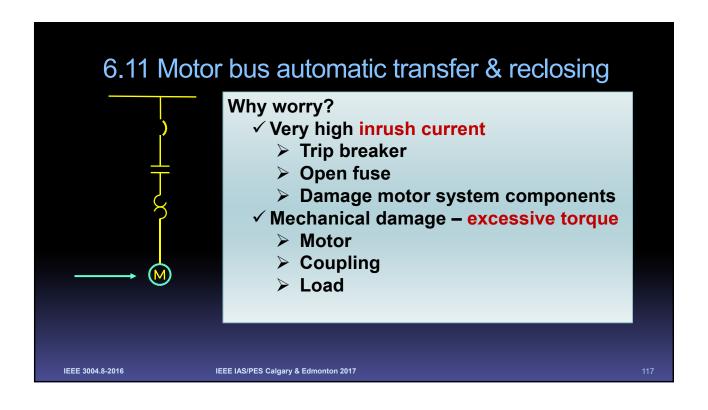
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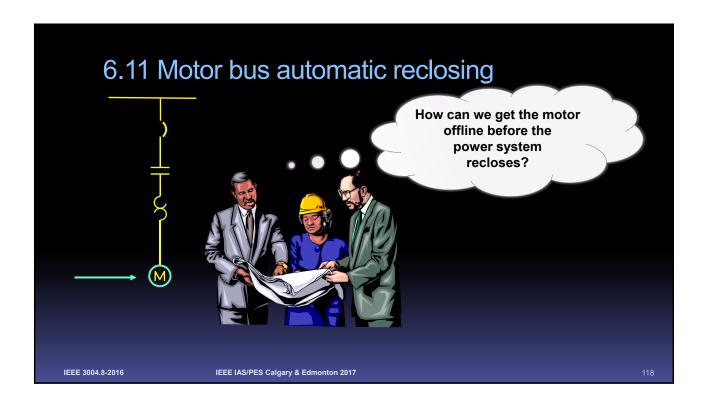
Other protection considerations

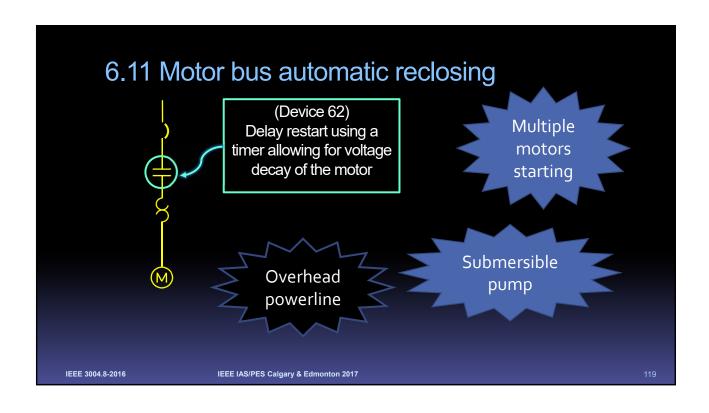
- Transition timing (incomplete sequence) for autotransformer and reactor starters
- Controllers where two or more sets of CTs are used special consideration required for protection
 - Multispeed motors
 - Some Wye Delta configurations
- PF Capacitors

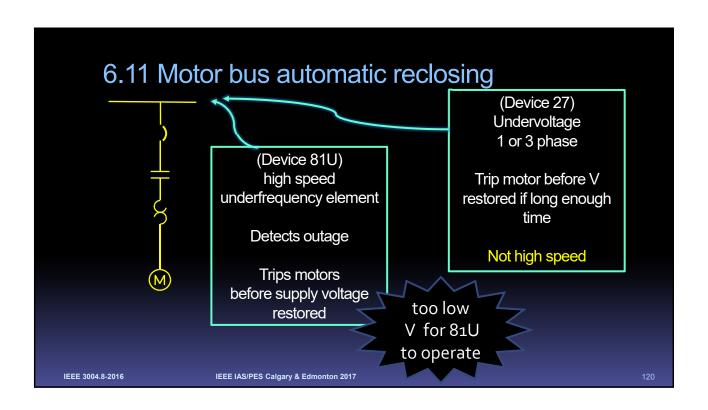
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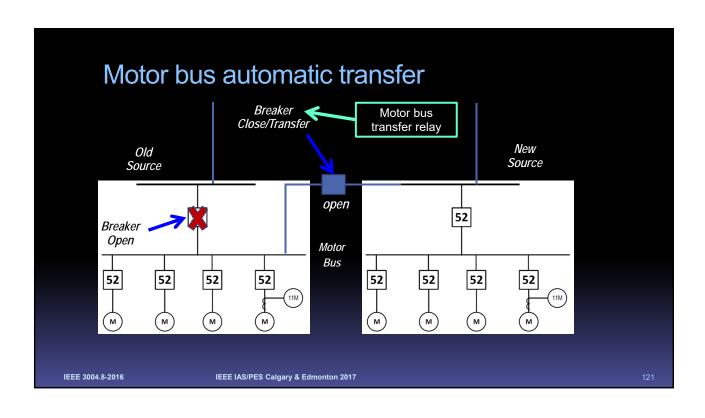
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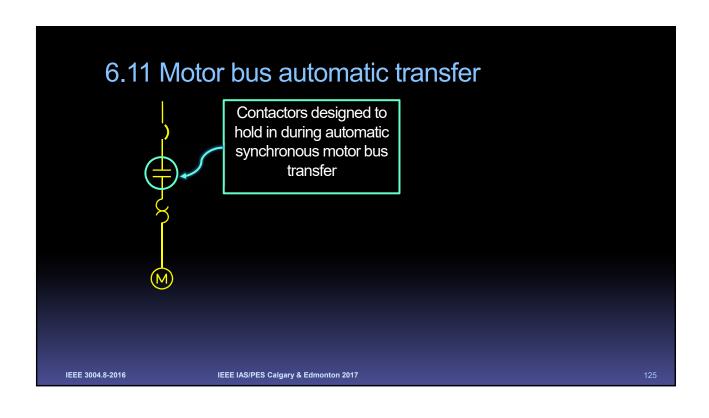


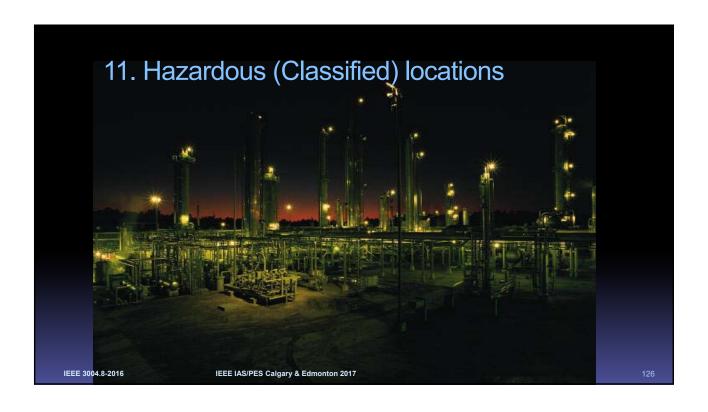




МВТ	Old Source Breaker	New Source Breaker	Supervised	Unsupervised
Open-transition transfer	Open	Open		
Fast transfer – supervised	Open	Open	Voltage phase angle (synch-check)	
Fast transfer – unsupervised	Open	Open		No synch-check or slow synch-check
In-phase transfer	Open	Open	Close command compensates for breaker close time	
Residual voltage transfer	Open	Open	New Breaker close command after voltage on Old Source is low enough	No sych-check
Sequential transfer (fast, in-phase, & sequential)	Open	Open	Close command supervised by open signal from Old Source Breaker	

МВТ	Old Source Breaker	New Source Breaker	Supervised	Unsupervised
Simultaneous transfer (fast, in-phase, & sequential)	Open	Open		No verification the Old Source Breaker is open
Slow transfer	Open	Open	Verified Old Source Breaker open for >20 cycles; then close New Breaker	No synch-check No Voltage monitor
Synchronous bus transfer (fast transfer-supervised or in-phase)	Open	Open	Breaker close is supervised, voltage decay and frequency decay monitored to close New Breaker at or near zero phase coincidence	
Closed-transition transfer (parallel transfer)	Closed	Closed	(sych-check)	
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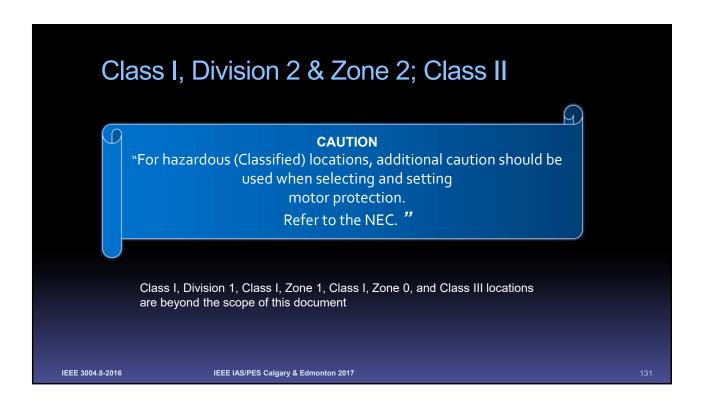








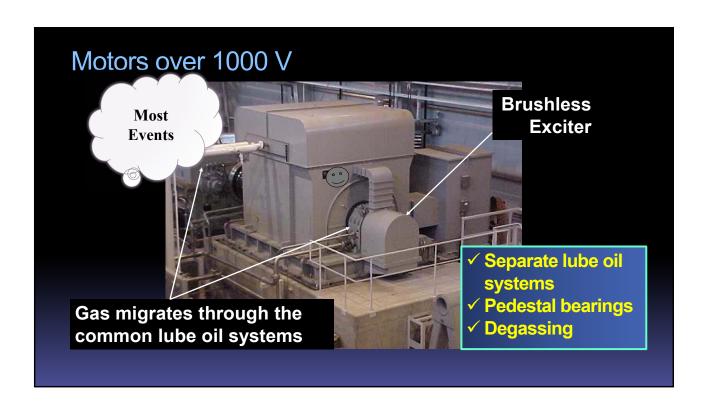


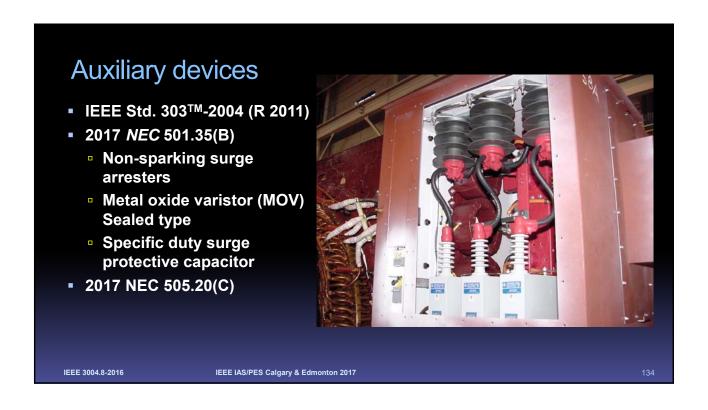


Overload

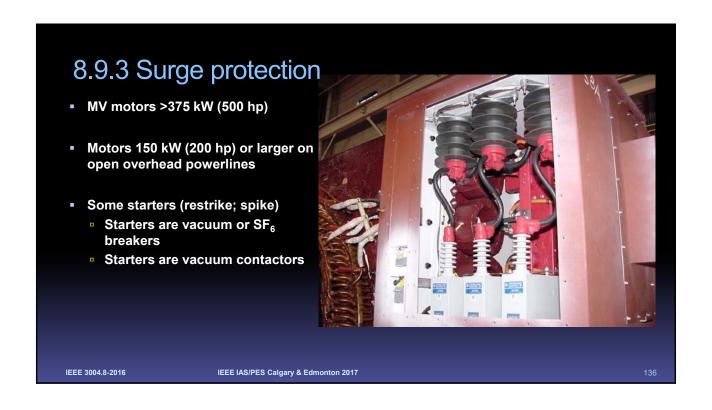
Select motor size to avoid overload condition

- Reference 2017 NEC
 - 430.32 continuous-duty motors
 - 430.124 ASD overload protection
 - 430.225(B) motors over 1000 V nominal
- Overload device settings
 - 115% or less of motor rated current
- ASD operating current limit
 100% of motor nameplate rated current

















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Figures 48, 49, 50, 51, 52, 53, and D.1 courtesy of Rockwell Automation.

Figures C.1, C.2, and C.3 and Table C.1 courtesy of HVPD

Figures D.2, D.3, and D.4 courtesy of DC Water.

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Daleep Mohla, Chair

(> 100 Formal Balloters)

I&CPS

Protection & Coordination Working Group

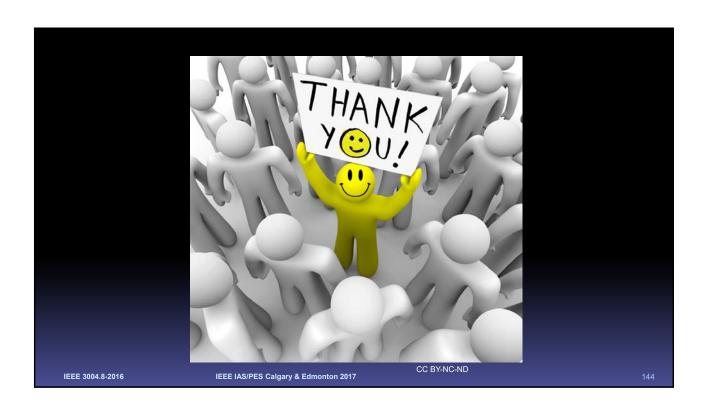
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